

# Performance estimation of a remote field eddy current method for the inspection of water distribution pipes

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**Québec**

# Degradation and renewal of water distribution pipes

- Replacement of water pipes: important expenditures
  - e.g. Burn et al. (2007): annual worldwide expenditure for water distribution pipes > US\$ 33,000 million/year
  - should rise significantly in the future as existing assets increasingly come to the end of their useful lives
- Most of small diameter pipes installed < 1990 = metallic (ductile or gray cast iron)



Source : <http://video.monteregie.hebdosregionaux.ca>



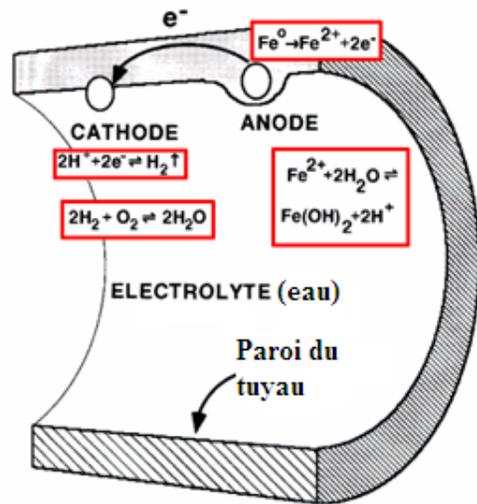
Source : <http://www.cfgservices.fr>

# Corrosion of water distribution pipes

Cast iron pipes (installation)



Corrosion over time



Tubercles  
(corrosion product)



External corrosion  
(here graphitic)



Hole in the pipe



# Consequences of corrosion

- Increased frequency / probability of pipe breaks and leaks
- Increased costs + interruptions in water supply
- Solutions :

- replace?
- repair?
- which pipes?
- when?



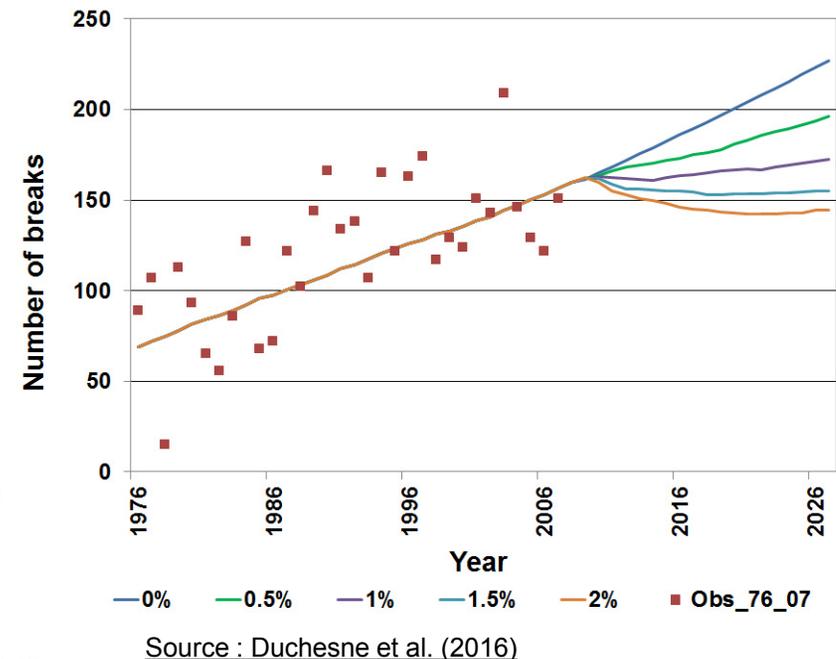
Source : <http://video.monteregie.hebdosregionaux.ca>



Source : <http://www.cfgservices.fr>

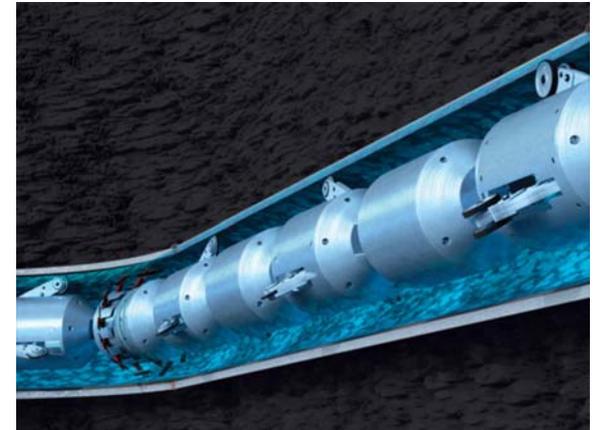
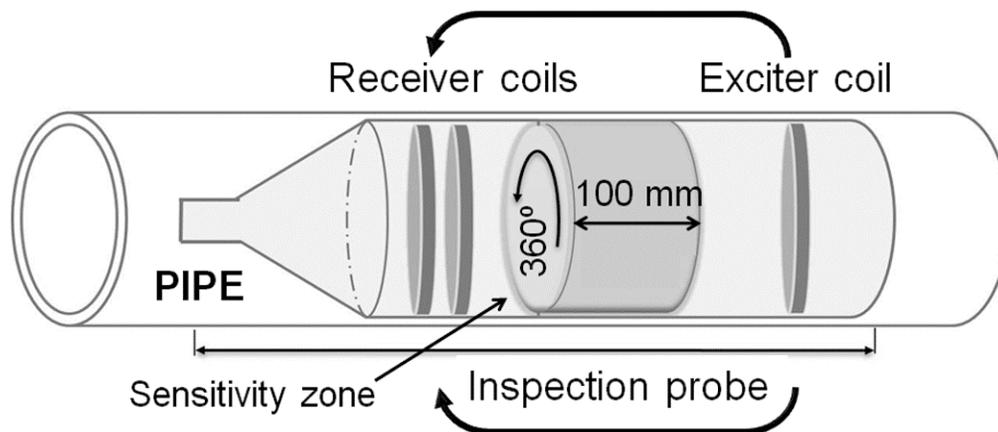
# Existing tools to plan the renewal

- Prediction models and planning tools:
  - assess the required financial resources
  - prioritizing pipes that should be replaced and/or rehabilitated
- Decision to replace / repair a specific pipe:
  - requires assessment of its conditions
    - observed breaks and leaks (indicators)
    - observations from inspection



# RFEC technique for the inspection of water distribution pipes

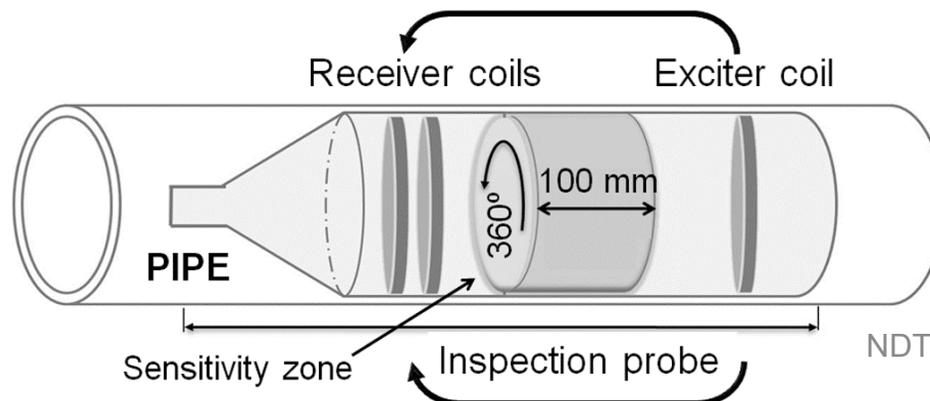
- Remote Field Eddy Current:
  - application well known for the identification and sizing of defects in metallic gas distribution pipes
  - can be applied to water distribution pipes



Source : <http://www.popsci.com/technology/article/2011-01/pig-robots-keep-gas-lines-blowing>

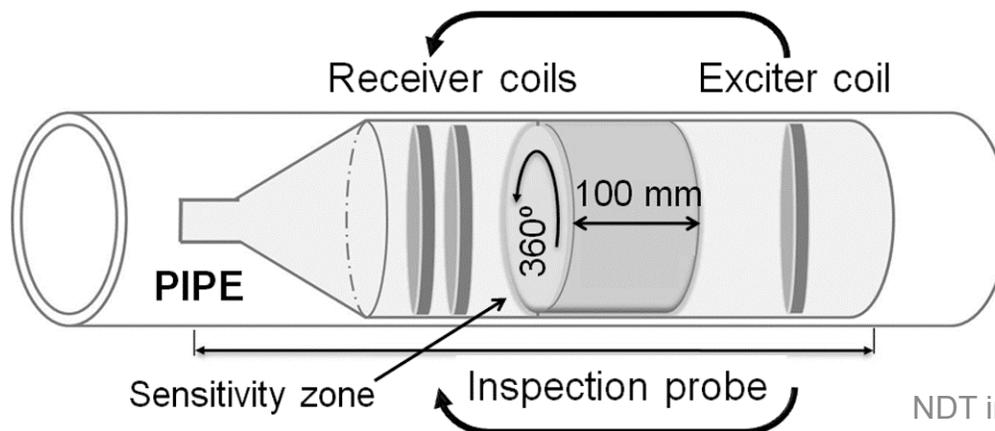
# RFEC technique for the inspection of water distribution pipes

- Exciter transmits a low frequency magnetic field that can reach receivers by two paths:
  1. inside the pipe through the water (direct path)
  2. through the outside of the pipe (indirect path)
- Strength of magnetic field attenuated rapidly in direct path
  - at  $\approx$  two pipe diameters from exciter, indirect field dominates the direct field: the remote field zone begins



# RFEC technique for the inspection of water distribution pipes

- Variations of wall thickness at the locations where the magnetic field goes through the pipe modify phase and/or amplitude of the signal
  - can be translated into wall thickness reduction and spatial extent of the detected flaw
- Does not measure the actual pipe-wall thickness: evaluation of the material loss percentage



# Objective and general methodology

Objective : Assess the performance of an existing RFEC probe for the inspection of cast iron water pipes

1. Inspect 6 pipes with the probe
2. Compare size and location of corrosion defects estimations with values resulting from the processing of computed tomography (CT) images of the same pipes



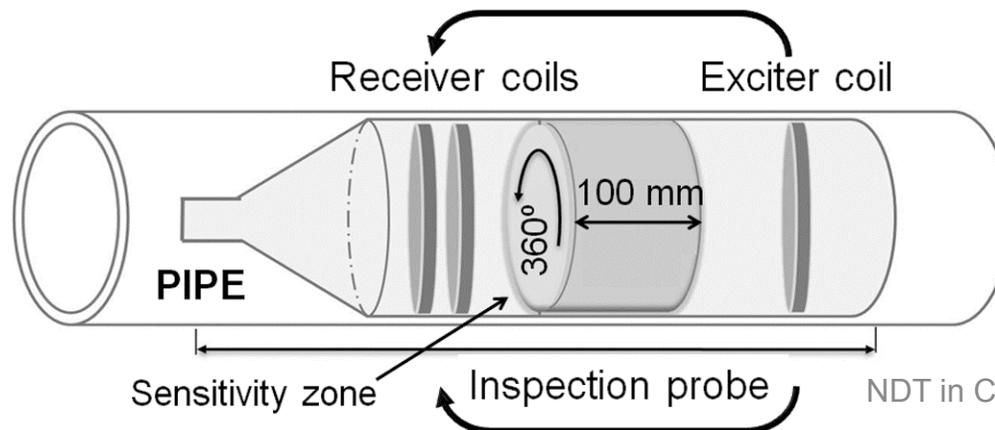
# Analyzed pipes (excavated)

	Estimated date of installation	Estimated age at inspection	Diameter	Length	Average wall thickness
		(years)	(mm)	(m)	(mm)
<b>NEW-PIPE</b>	-	-	150	1.1	7
<b>SILL-MAG-1A</b>	1948	61	200	1.6	14
<b>B-MAN-1A</b>	1909	100	150	2.6	10
<b>B-MAN-1B</b>	1909	100	150	2.5	10
<b>B-MAN-2A</b>	1909	100	150	1.7	12
<b>B-MAN-2B</b>	1909	100	150	1.7	9
<b>LHSTCH-MC</b>	1945	64	150	1.3	7
<b>LHSTCH-HOP</b>	1957	52	150	3.2	8

- RFEC probe passed once in each pipe (laboratory = air)
- Comparison with *in situ* inspection for one pipe

# Inspection results

	Defect	Location	Thickness loss	Sensitivity zone coverage
		(m)	(%)	(%)
B-MAN-1A	#1	1.2	22	22
B-MAN-1B	#1	0.8	17	13
	#2	1.6	28	17
B-MAN-2A	#1	1.8	15	63
B-MAN-2B	#1	0.4	23	< 13
	#2	1.3	26	13
LHSTCH-MC	#1	0.7	38	24
LHSTCH-HOP	#1	1.4	20	< 13



# Condition evaluation with the CT scan

- Based on Lambert-Beer law:

$$N = N_0 e^{-\mu x}$$

$N$  = measured intensity after layer of thickness  $x$ ;

$N_0$  = incident radiation intensity (usually in keV);

$\mu$  = linear attenuation coefficient → depends linearly on the density of the material

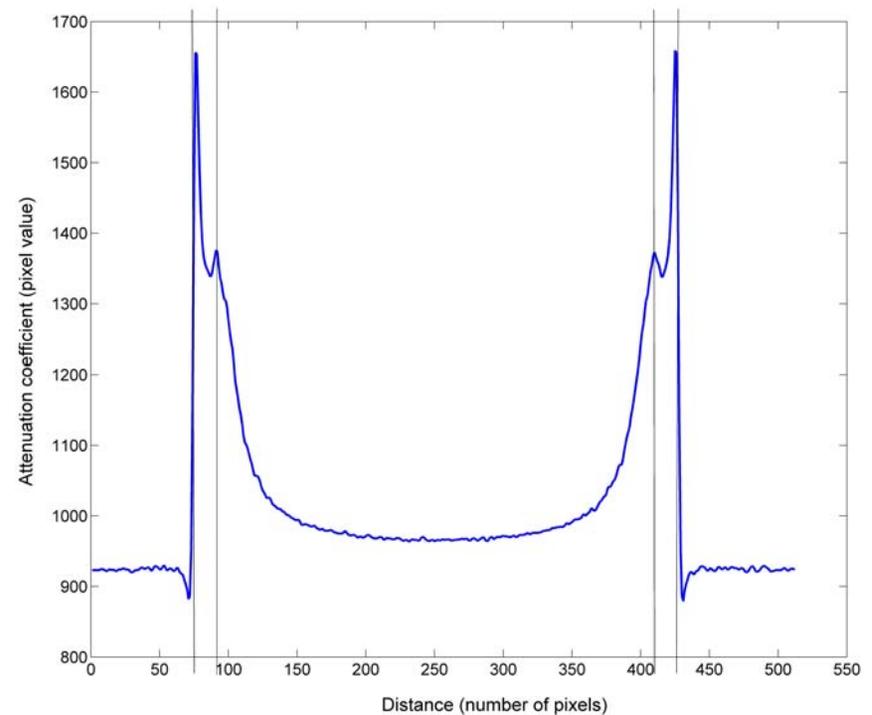
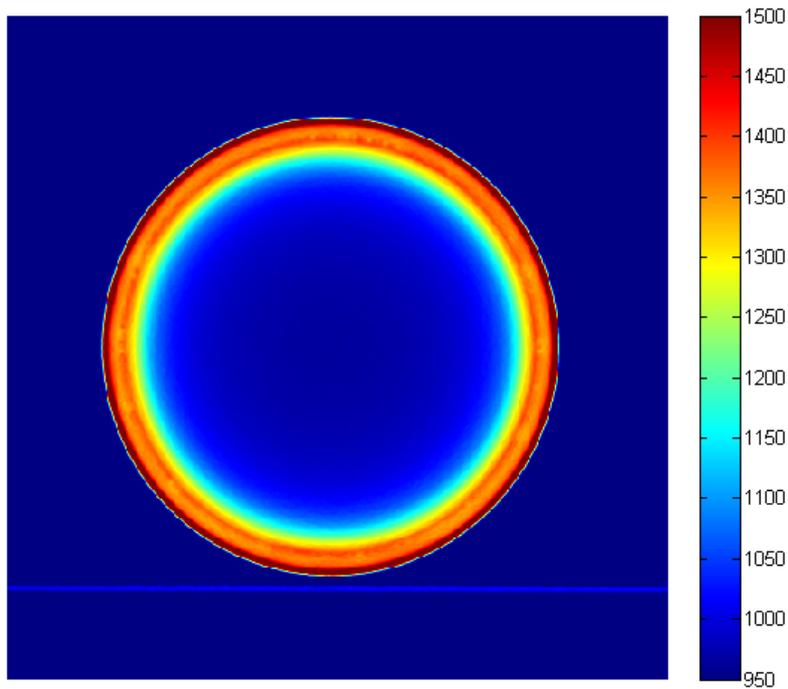
- Output from CT scan computer:

$$HU = \frac{\mu - \mu_{water}}{\mu_{water}} \times 1000$$

- When viewed in Matlab:

$$pixel\_value = \frac{HU + 10240}{10}$$

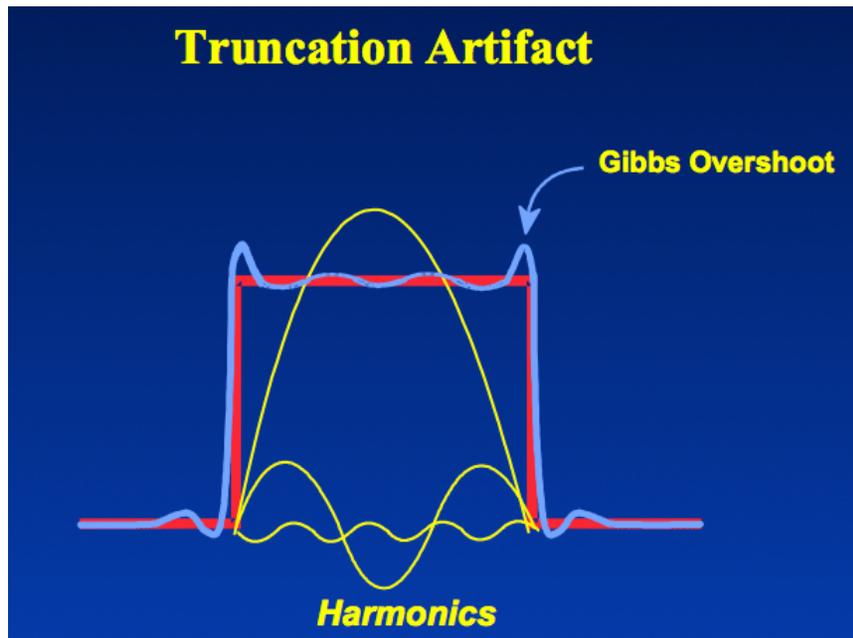
# Condition evaluation with the CT scan



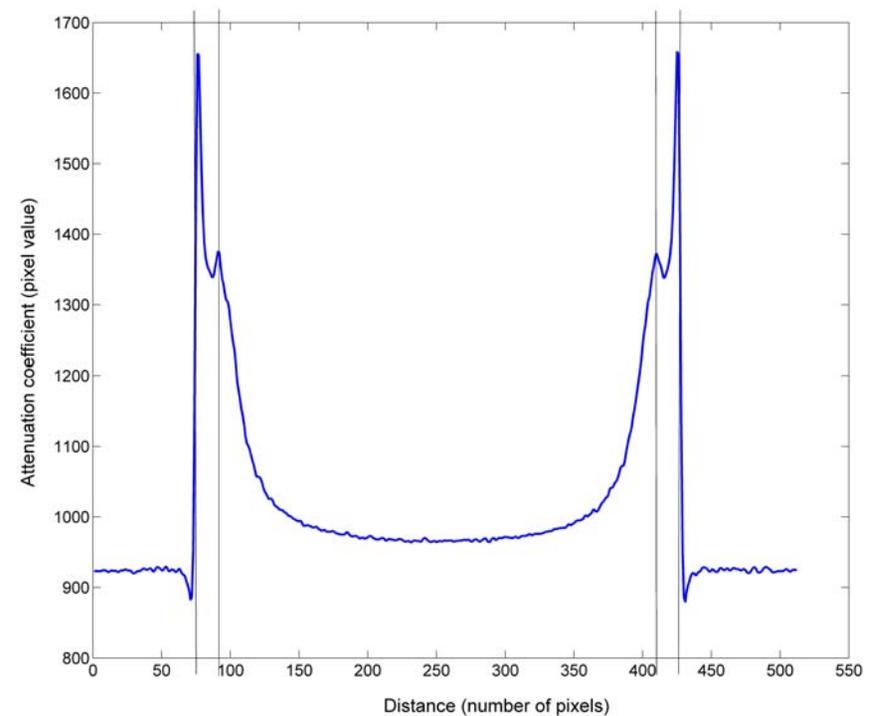
- When viewed in Matlab:

$$pixel\_value = \frac{HU + 10240}{10}$$

# Condition evaluation with the CT scan



Source: <http://mriquestions.com/gibbs-artifact.html>

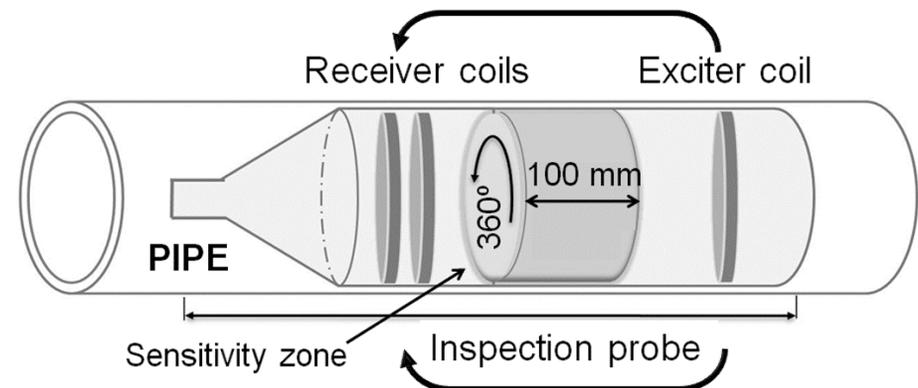


- When viewed in Matlab :

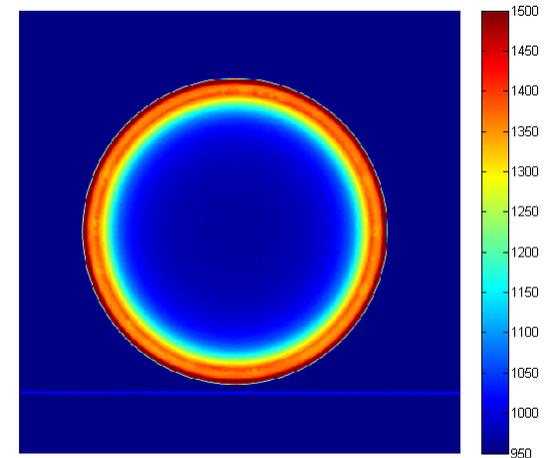
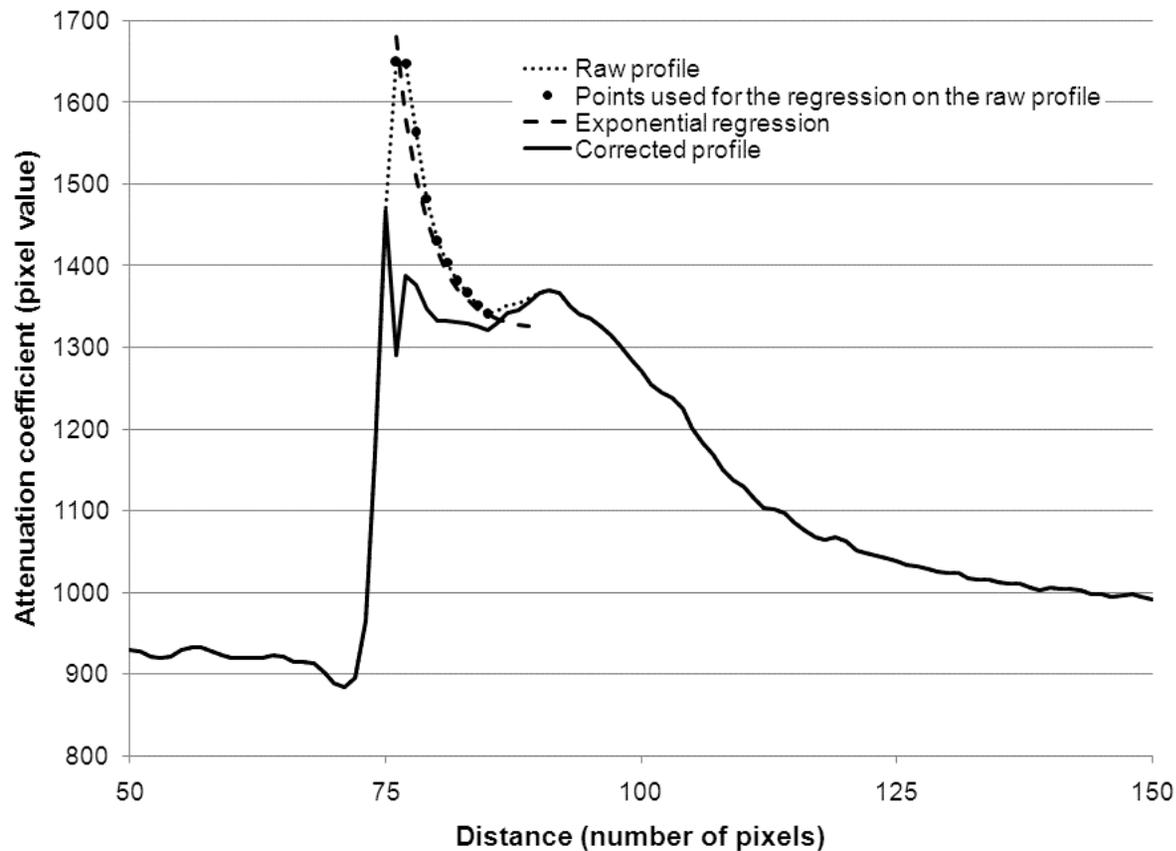
$$pixel\_value = \frac{HU + 10240}{10}$$

# Condition evaluation with the CT scan

- Objective, to compare with the RFEC tool:
  1. pipe thickness loss = percentage of lost material on 100 mm sensitivity zones, all along the pipes
  2. spatial extent of this loss
- Steps :
  1. Correction of artifacts
  2. Estimation of the mean percentage of material loss for 100 mm by 360° zones
  3. Estimation of the worst percentage of material loss on specific proportions of these  
15 100 mm by 360° sensitivity zones



# Correction of artifacts



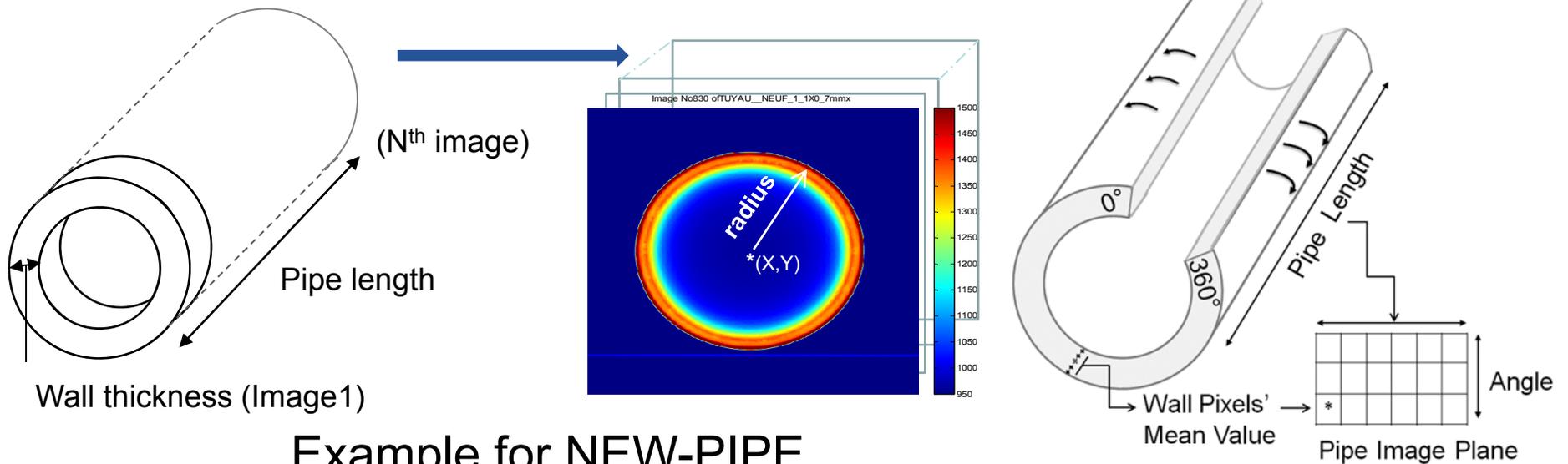
$$pv_{reg} = A + B \exp(-Cx)$$

$$\Delta pv = B \exp(-Cx)$$

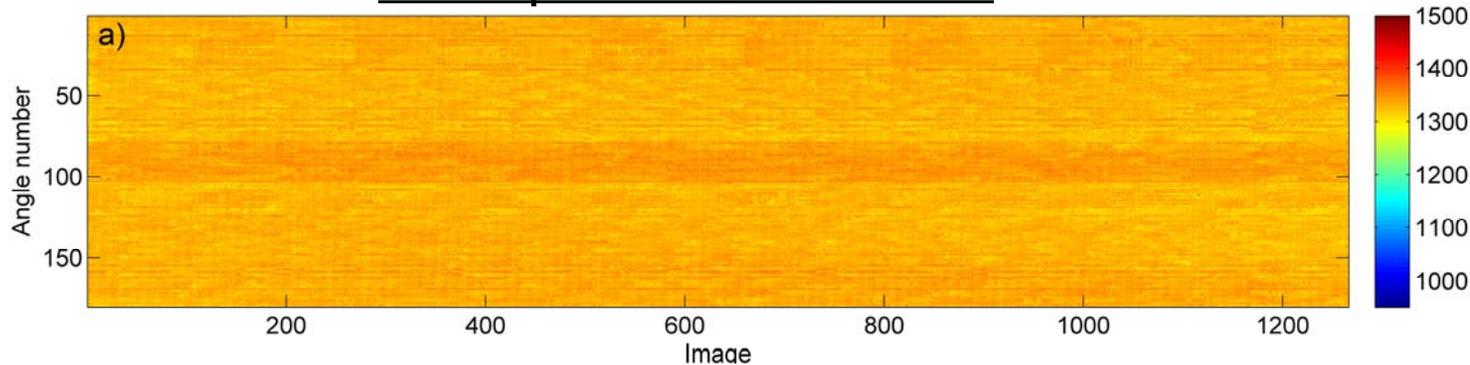
$$pv_{corr} = pv - \Delta pv$$

# Estimation of mean percentage of material loss

- Compute mean corrected pixel value across the pipe wall for 180 different angles ( $2^\circ$  apart)

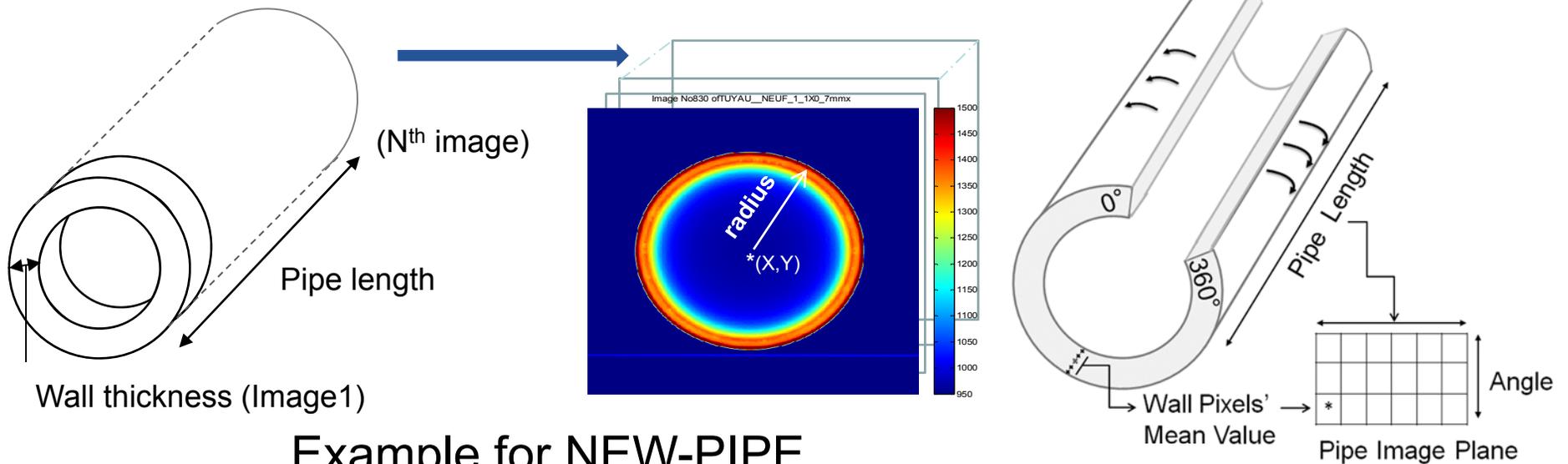


## Example for NEW-PIPE

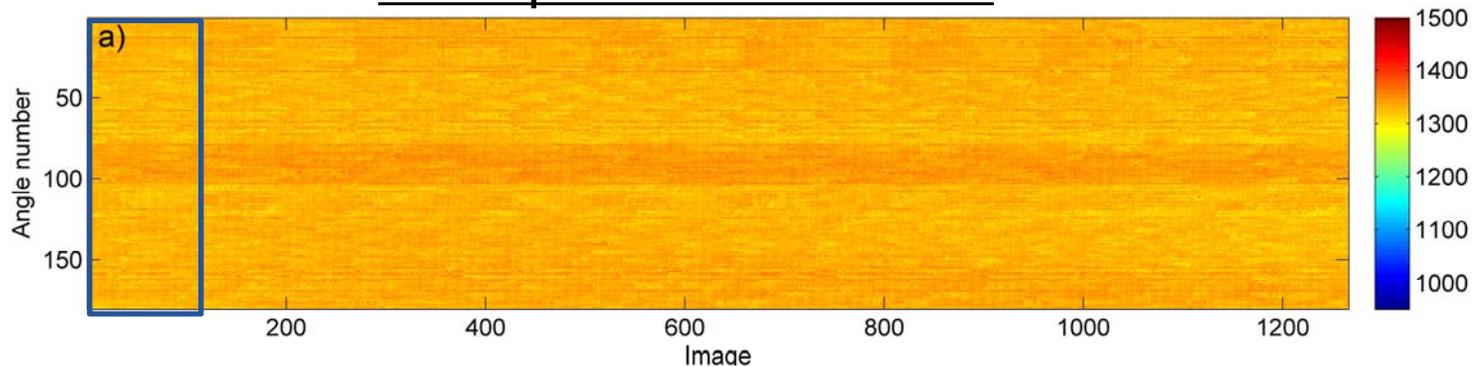


# Estimation of mean percentage of material loss

- Compute mean corrected pixel value across the pipe wall for 180 different angles ( $2^\circ$  apart)



## Example for NEW-PIPE

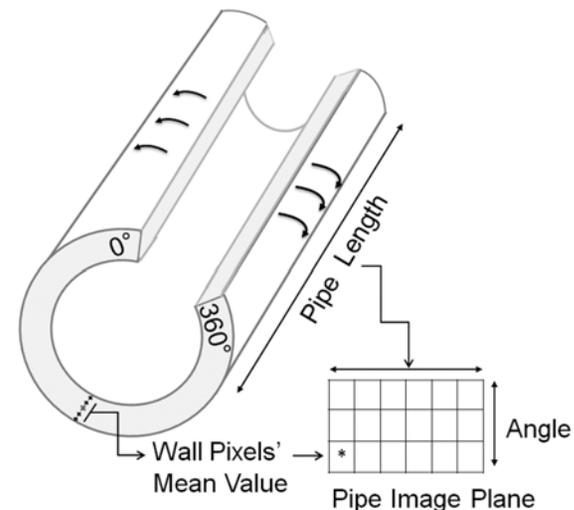
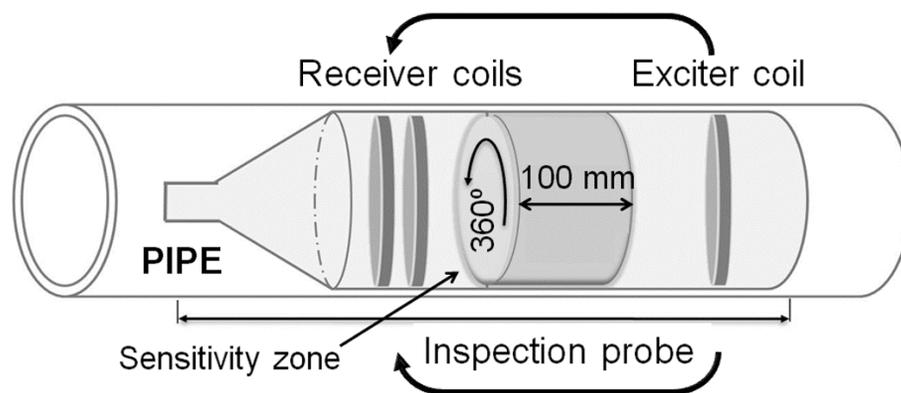


# Estimation of mean percentage of material loss

ii. Compute percentage of pipe-wall loss for each pixel

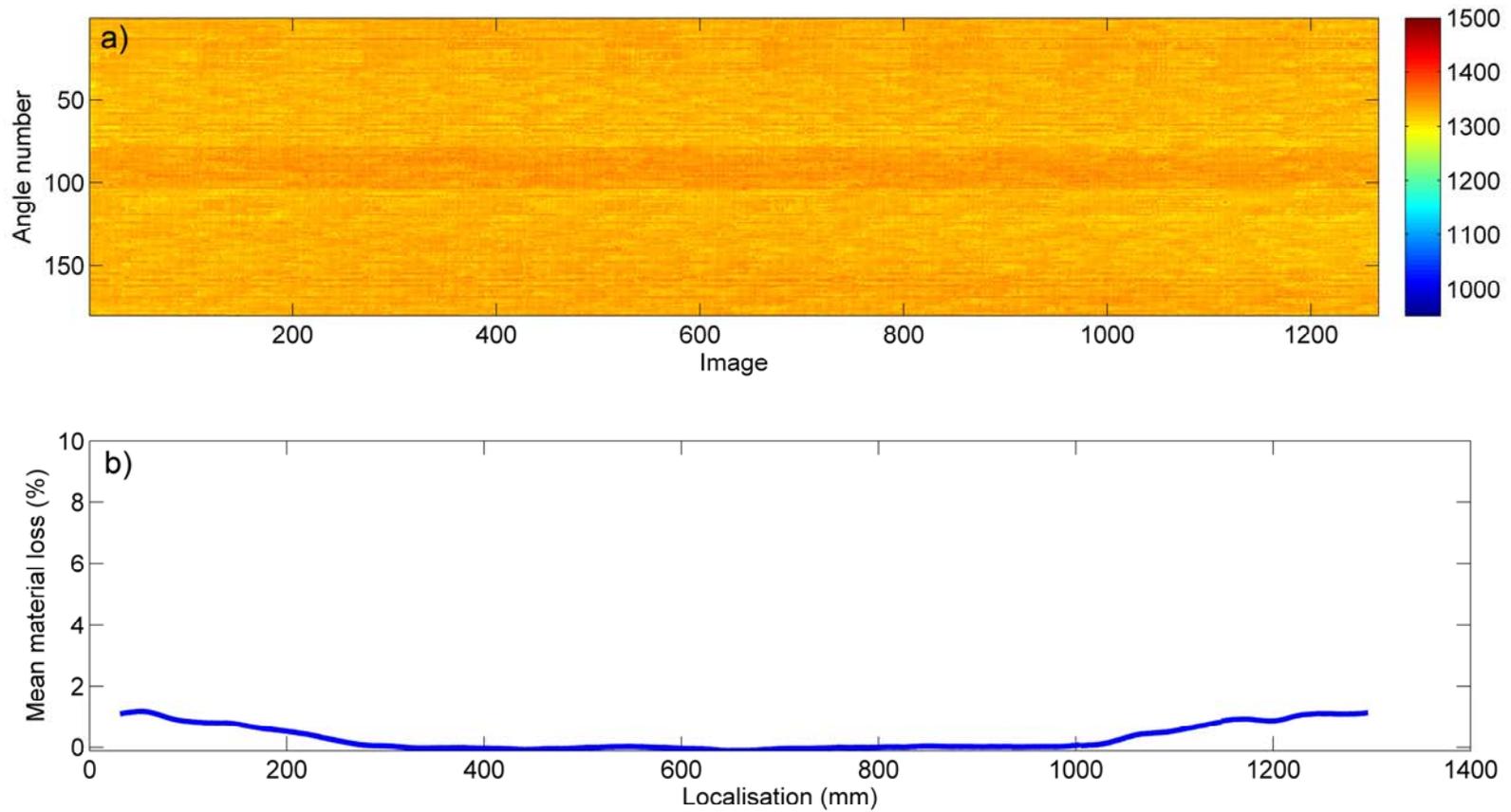
$$\%loss = \left[ 1 - \left( \frac{pv - pv_{\min}}{pv_{\max} - pv_{\min}} \right) \right] \times 100$$

iii. Average the percentage of material loss (for 100-mm strips) over all 180 - 2° angles (360°)



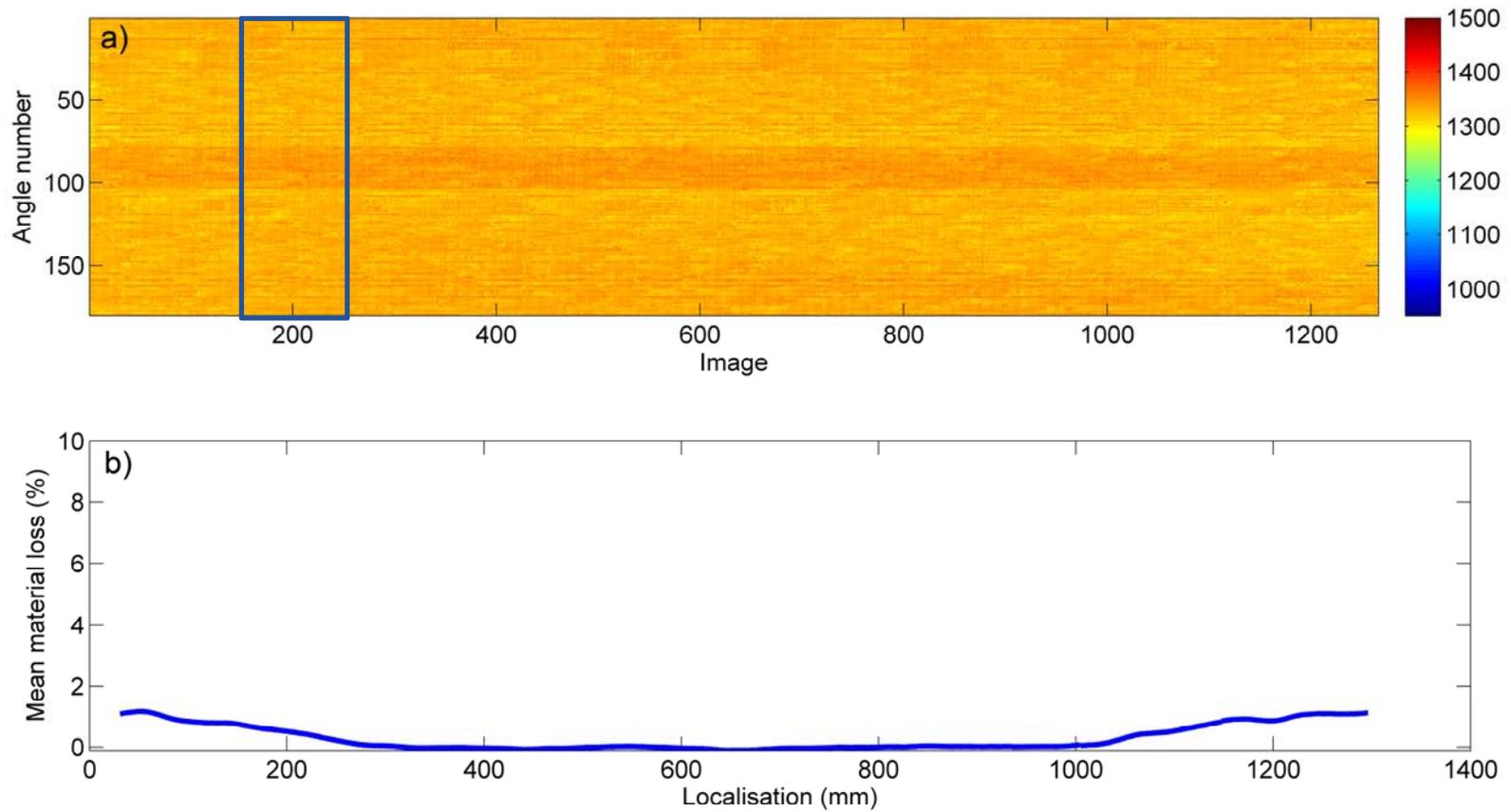
# Estimation of mean percentage of material loss

## Example for NEW-PIPE



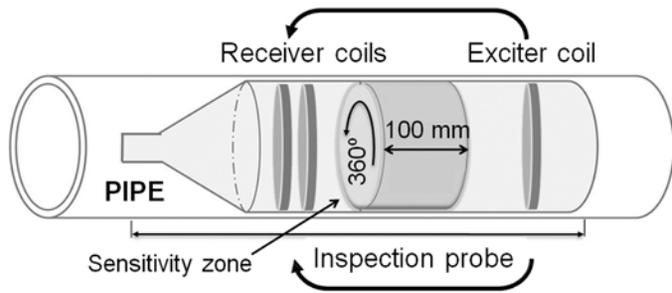
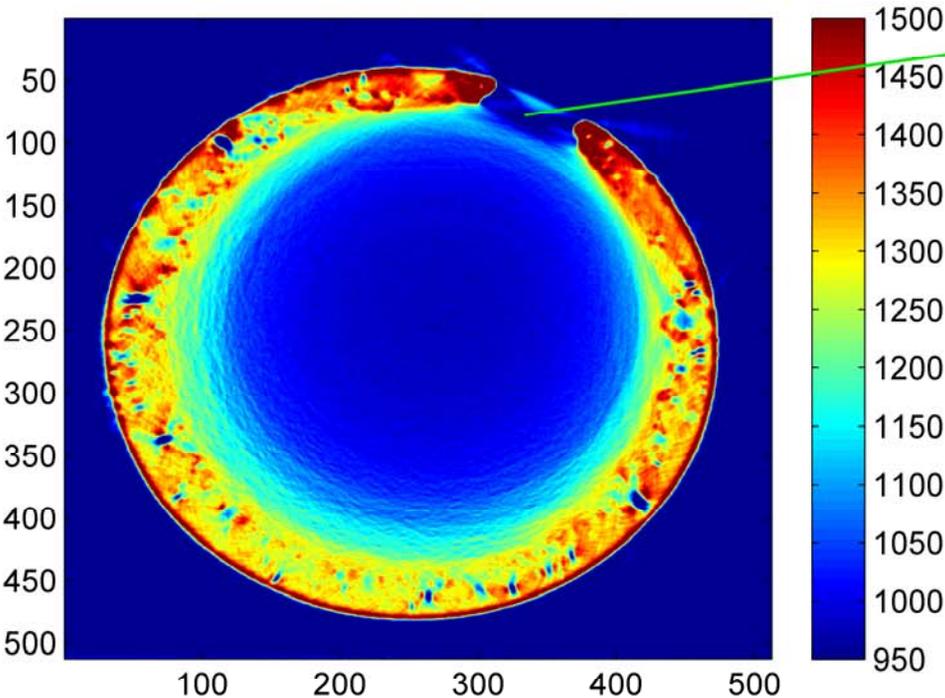
# Estimation of mean percentage of material loss

## Example for NEW-PIPE



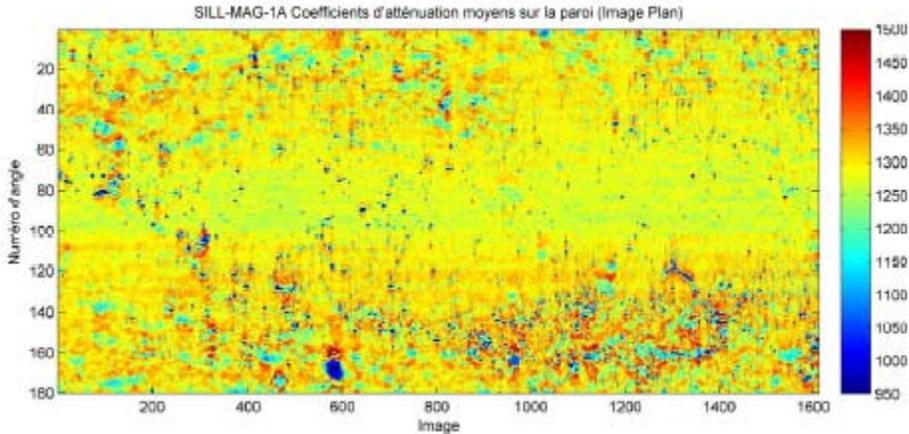
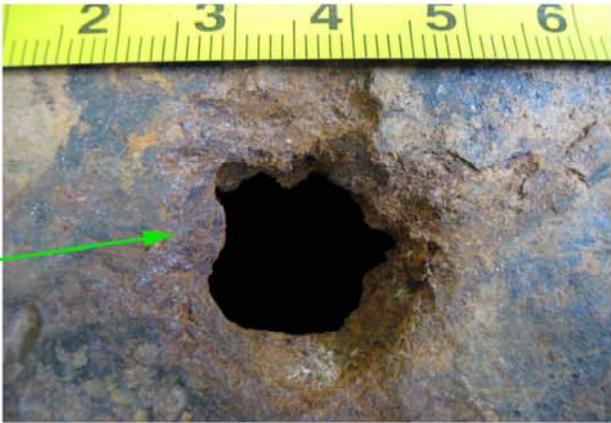
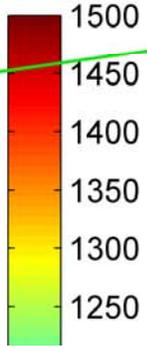
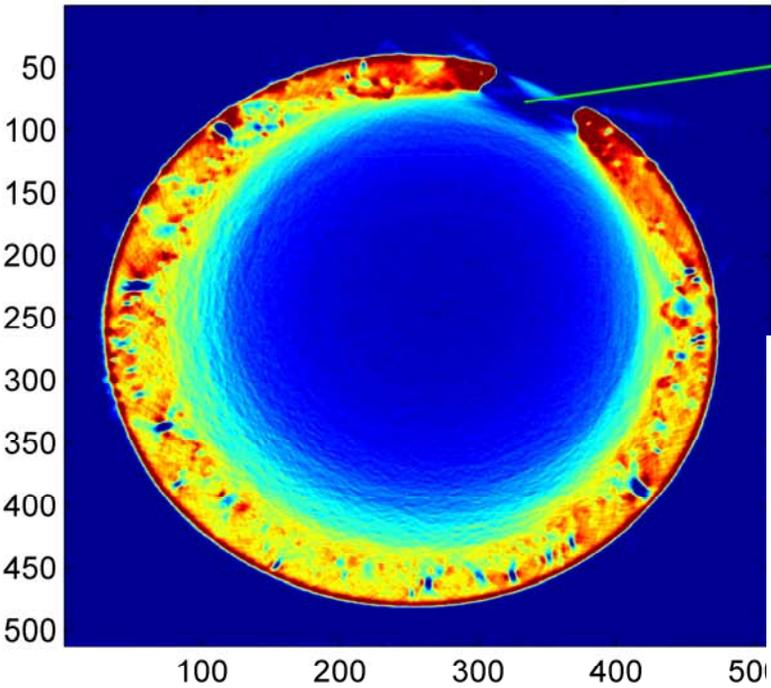
# Estimation of worst thickness loss

Example for SILL-MAG-1A



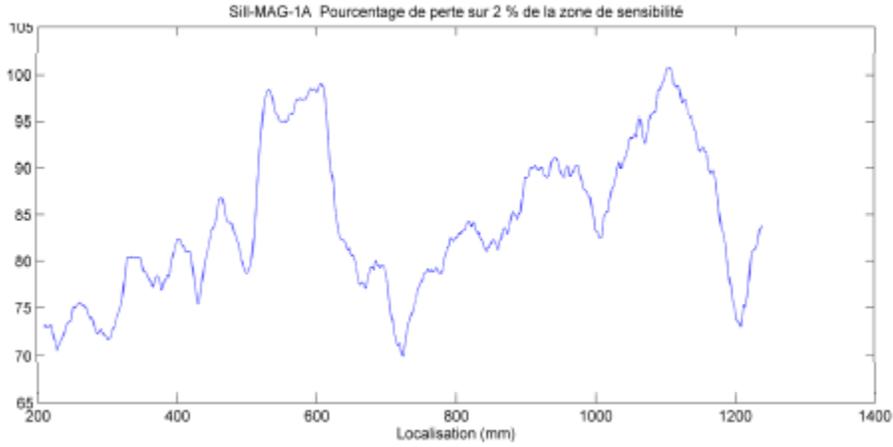
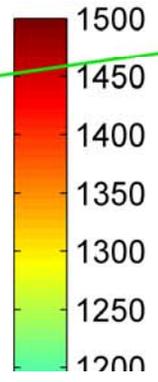
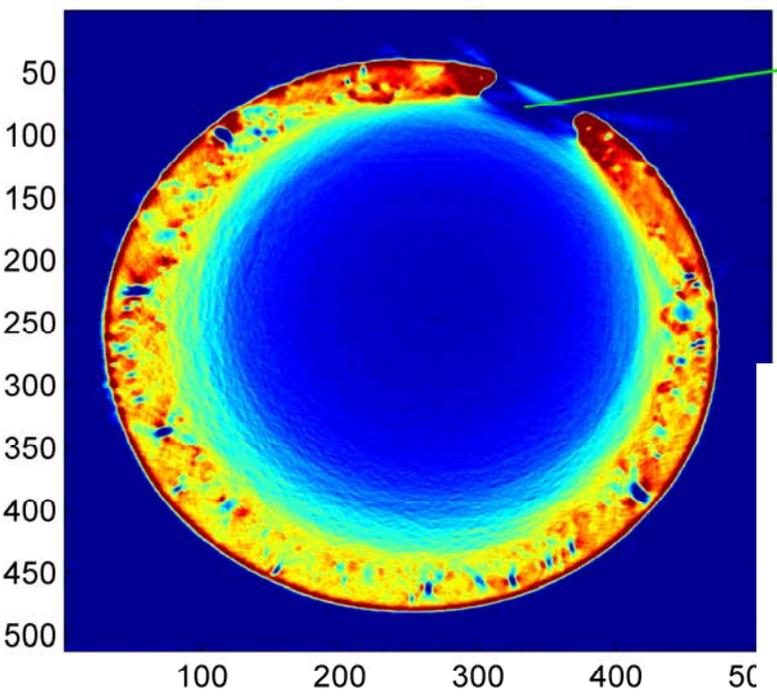
# Estimation of worst thickness loss

## Example for SILL-MAG-1A



# Estimation of worst thickness loss

Example for SILL-MAG-1A



# Summary of results

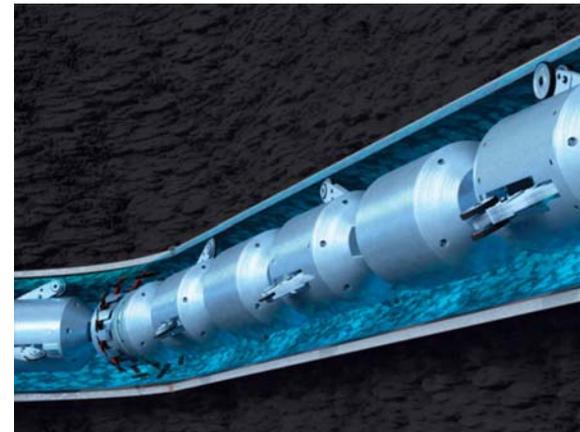
Pipe	Defect	CT scan image analysis			RFEC Tool		
		Location (m)	Thickness loss (%)	Sensitivity zone coverage (%)	Location (m)	Thickness loss (%)	Sensitivity zone coverage (%)
B-MAN-1A	#1	0.7	18	13	n.i.	n.i.	n.i.
	#2	1.3	22	22	1.2	22	22
B-MAN-1B	#1	0.7 - 0.9	16	13	0.8	17	13
	#2	1.6	15	17	1.6	28	17
B-MAN-2A	#1	0.8	34	13	n.i.	n.i.	n.i.
	#2	1.2 - 1.5	14	63	1.8	15	63
B-MAN-2B	#1	0.4	20	13	0.4	23	< 13
	#2	1	25	13	n.i.	n.i.	n.i.
	#3	1.4	48	13	1.3	26	13
LHSTCH-MC	#1	0.1	27	13	n.i.	n.i.	n.i.
	#2	0.7	20	24	0.7	38	24
LHSTCH-HOP	#1	0.2	17	13	n.i.	n.i.	n.i.
	#2	1.4	12	13	1.4	20	< 13

n.i.: not identified

# Conclusions

- Similar results for both techniques:
  - but RFEC tool: thickness loss  $\geq 15\%$  when averaged on the 13% most corroded area of the tool's sensitivity zone
- RFEC tool provides reliable information on the main corrosion defects and thus on the general structural state of water pipes
- RFEC tool cannot identify small corrosion pits:
  - could cause leaks and even initiate larger corrosion areas
  - better detected by leak detection methods (e.g. acoustic)
- Further tests required (more pipes, lined or coated pipes, ductile iron pipes)

# Questions ?



Source : <http://www.popsci.com/technology/article/2011-01/pig-robots-keep-gas-lines-blowing>

Name	Pixel size (mm)	Slice thickness	Spacing between slices
		(mm)	(mm)
<b>NEW-PIPE</b>	0.492	1	0.7
<b>SILL-MAG-1A</b>	0.517	1	0.7
<b>B-MAN-1A</b>	0.492	1	0.7
<b>B-MAN-1B</b>	0.492	1	0.7
<b>B-MAN-2A</b>	0.492	1	0.7
<b>B-MAN-2B</b>	0.492	1	0.7
<b>LHSTCH-MC</b>	0.449	1	0.7
<b>LHSTCH-HOP</b>	0.431	1	1.0

